

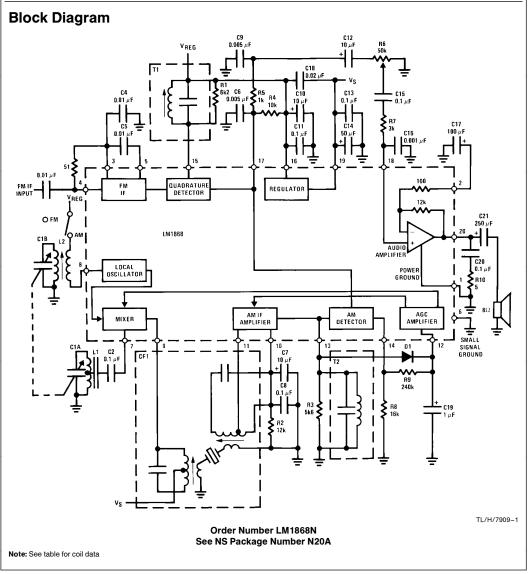
# LM1868 AM/FM Radio System

# **General Description**

The combination of the LM1868 and an FM tuner will provide all the necessary functions for a 0.5 watt AM/FM radio. Included in the LM 1868 are the audio power amplifier, FM IF and detector, and the AM converter, IF, and detector. The device is suitable for both line operated and 9V battery applications.

## **Features**

- DC selection of AM/FM mode
- Regulated supply
- Audio amplifier bandwidth decreased in AM mode, reducing amplifier noise in the AM band
- AM converter AGC for excellent overload characteristics
- Low current internal AM detector for low tweet radiation



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# **Absolute Maximum Ratings**

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/Distributors for availability and specifications.

Supply Voltage (Pin 19) 15V Package Dissipation 2.0W

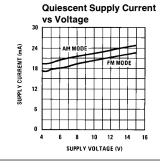
Above  $T_A = 25^{\circ}\text{C}$ , Derate Based on  $T_{\text{J(MAX)}} = 150^{\circ}\text{C}$  and  $\theta_{\text{JA}} = 60^{\circ}\text{C/W}$ 

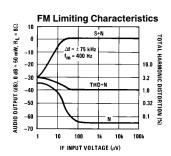
 $\begin{array}{lll} \mbox{Storage Temperature Range} & -55^{\circ}\mbox{C to } + 150^{\circ}\mbox{C} \\ \mbox{Operating Temperature Range} & 0^{\circ}\mbox{C to } + 70^{\circ}\mbox{C} \\ \mbox{Lead Temperature (Soldering, 10 sec.)} & 260^{\circ}\mbox{C} \\ \end{array}$ 

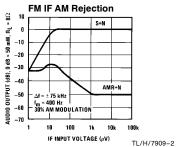
# **Electrical Characteristics** Test Circuit, $T_A = 25^{\circ}C$ , $V_S = 9V$ , $R_L = 8\Omega$ (unless otherwise noted)

Parameter	Conditions	Min	Тур	Max	Units
STATIC CHARACTERISTICS $e_{AM}=0$ ,	e <sub>FM</sub> = 0				
Supply Current	AM Mode, S1 in Position 1		22	30	mA
Regulator Output Voltage (Pin 16)		3.5	3.9	4.8	V
Operating Voltage Range		4.5		15	
DYNAMIC CHARACTERISTICS—AM M $f_{AM}=1$ MHz, $f_{mod}=1$ kHz, 30% Modu	<b>ODE</b> lation, S1 in Position 1, $P_O = 50$ mW unless	s noted			
Maximum Sensitivity	$\begin{array}{l} \text{Measure e}_{\text{AM}}  \text{for P}_{\text{O}} = 50  \text{mW}, \\ \text{Maximum Volume} \end{array}$	8		16	μV
Signal-to-Noise	e <sub>AM</sub> = 10 mV	40	50		dB
Detector Output	e <sub>AM</sub> = 1 mV Measure at Top of Volume Control	40	60	85	mV
Overload Distortion	e <sub>AM</sub> = 50 mV, 80% Modulation		2	10	%
Total Harmonic Distortion (THD)	e <sub>AM</sub> = 10 mV		1.1	2	%
DYNAMIC CHARACTERISTICS—FM M	<b>ODE</b> $f_{FM} = 10.7 \text{ MHz}, f_{mod} = 400 \text{ Hz}, \Delta f =$	= ±75 kHz,	$P_0 = 50 \text{ m}$	W, S1 in Pos	ition 1
−3 dB Limiting Sensitivity			15	45	μV
Signal-to-Noise Ratio	e <sub>FM</sub> = 10 mV	50	64		dB
Detector Output	$e_{FM}=$ 10 mV, $\Delta f=\pm 22.5$ kHz Measure at Top of Volume Control	40	60	85	mV
AM Rejection	e <sub>FM</sub> = 10 mV, 30% AM Modulation	40	50		dB
Total Harmonic Distortion (THD)	e <sub>FM</sub> = 10 mV		1.1	2	%
DYNAMIC CHARACTERISTICS—AUDI	O AMPLIFIER ONLY $f = 1 \text{ kHz}, e_{AM} = 0, e_{AM} = 0$	e <sub>FM</sub> = 0, S1	in Position	2	•
Power Output	$THD = 10\%, R_L 8\Omega$ $V_S = 6V$ $V_S = 9V$	250 500	325 700		mW mW
Bandwidth	AM Mode, $P_O = 50 \text{ mW}$ FM Mode, $P_O = 50 \text{ mW}$		11 22		kHz kHz
Total Harmonic Distortion (THD)	P <sub>O</sub> = 50 mW, FM Mode		0.2		%
Voltage Gain			41		dB

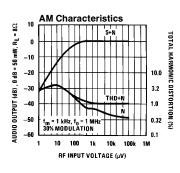
# Typical Performance Characteristics (Test Circuit) All curves are measured at audio output

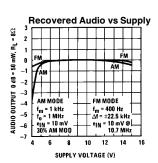


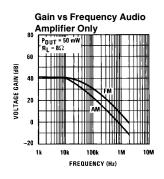


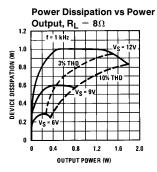


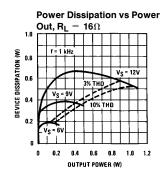
# Typical Performance Characteristics (Continued) All curves are measured at audio output (Test Circuit)

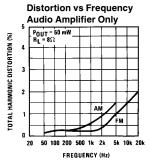






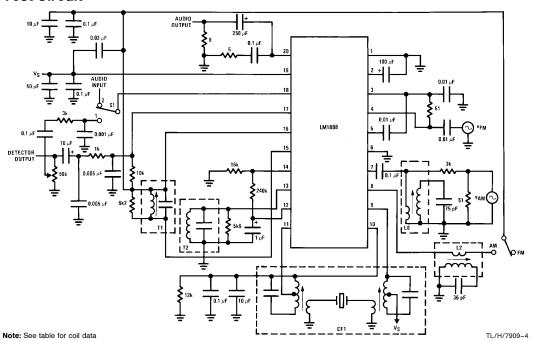


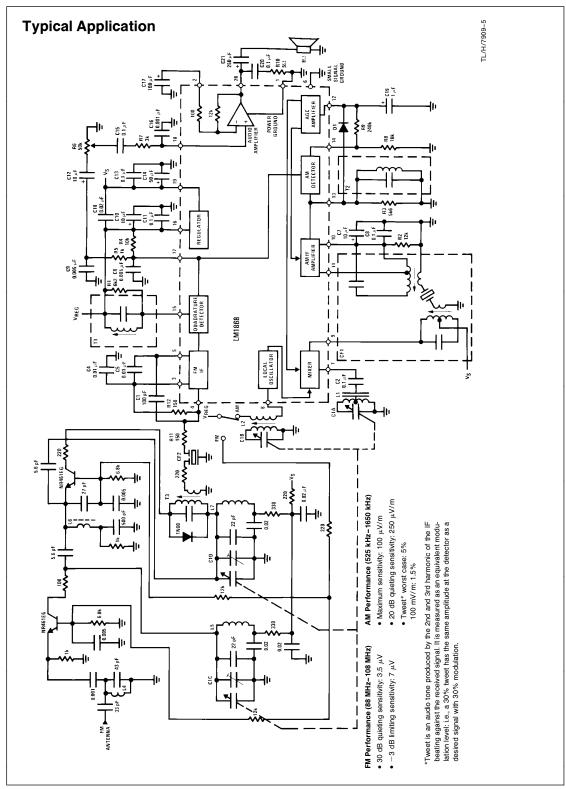




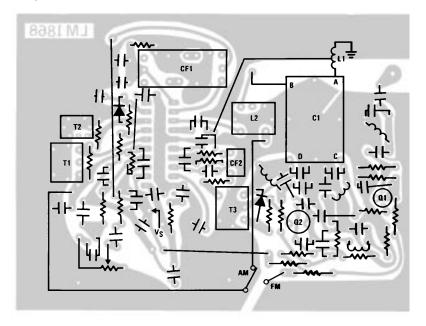
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# **Test Circuit**





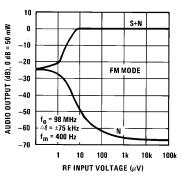
# **PC Board Layout**



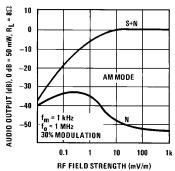
**Component Side** 

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# Typical Performance Characteristics Typical Application All curves are measured at audio output



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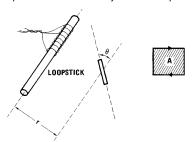
Value		Comments	Component	Typical Value	Comments	
100 pF	Remov	es tuner LO from IF input	R9	240k	Set AGC time constant	
0.1 μF	Antenr	na coupling capacitor	C19	1 μF		
0.01 μF	FM IF	decoupling capacitors	C7	10 μF	IF coupling	
$0.005 \mu\text{F}$ )	AM sm	oothing/FM de-emphasis	C8	0.1 μF	IF coupling	
1k ∫			C20	0.1 μF )	High frequency load for audio	
	•		R10	$5\Omega$	amplifier, required to stabilize audio amplifier	
	11 ≃ -	(00 + 00) ( R4 R6 )	C21	250 μF	Output coupling capacitor	
10 "F		(111 - 110)	R1	6k2	Sets Q of quadrature coil, determining FM THD and	
	•				recovered audio	
•	•		R2	12k	IF amplifier bias R	
•		· -	R3	5k6	Sets gain of AM IF and Q of A	
•					IF output tank	
'			R4	10k	Detector load resistor	
		· · · · · ·	R6	50k	Volume control	
}			C18	0.02 μF	Power supply decoupling	
0.001 μF ) 100 μF	Power	amplifier feedback	R11, R12	150 $\Omega$	Terminates the ceramic filter, biases FM IF input stage	
supply r		rejection	D1	1N4148	Optional. Quickens the AGC response during turn on	
@ F = 796 kH: dary)		AM antenna 1 mV/meter induces approximately 100 μV open circuit at the secondary TOKO BWO-645105 or	الح		F	
987		requivalent Toko America 1250 Feehanville Drive Mount Prospect, IL 60056 (312) 297-0070	T2	Ÿ	Q <sub>u</sub> > 14 @ 455 kHz, L to resonate w/180 pF @ 455 kHz TOKO 159GC-A3785 or equivalent	
, N = 3½T, inr				TL/H/7909-11		
, N = 31/ <sub>2</sub> T, inr	ner		∪⊦1 <b>⊘80T ?</b>	<sup>38</sup>	TOKO CFU-090D or equivalen BW > 4.8 kHz @ 455 kHz	
			<u>76</u>	E 101 3 6	7.0	
= 5 mm	ner		<u> </u>	I /H/7909-12	13T	
SFE 10.7 mA o	r	Murata 2200 Lake Park Drive Smyrna, GA 30080 (404) 436-1300	T3 o 51 p	F 14T 11T 11T 11T 11T 11T 11T 11T 11T 11T	Apollo Electronics NS-107C or equivalent	
	0.1 μF 0.01 μF 0.005 μF 1 k 10 μF 0.1 μF 10 μF 0.1 μF 10 μF 0.1 μF 3 k 0.001 μF 100 μF 16 k Tuning 40 pF max 5.0 p 5 pF 10 μ = 200 c 12 pF max 5.0 p 5 pF 10 μ = 200 c 12 pF max 5.0 p 13 pF max 5.0 p 14 pF max 5.0 p 15 pF max 5.0 p 16 pF max 5.0 p 17 μ = 200 c 18 pF max 5.0 p 18 pF max 5.0 p 19 pF max 5.0 p 10 μ = 200 c 10 μ = 200 c	0.1 μF Antenn 0.01 μF FM IF 0 0.005 μF AM sm networ given b 1k	0.1 μF 0.01 μF 0.01 μF 0.005 μF 1k $ \begin{cases} 1 & = \frac{1}{2\pi \left(\text{C6} + \text{C9}\right) \left(\frac{\text{R4}}{\text{R4} + \text{R6}}\right)} \\ 1 & = \frac{1}{2\pi \left(\text{C6} + \text{C9}\right) \left(\frac{\text{R4}}{\text{R4} + \text{R6}}\right)} \\ 10 μF Regulator decoupling capacitor 0.1 μF Regulator decoupling capacitor 0.0 μF Regulator decoupling capacitor 0.1 μF Power supply decoupling 0.1 μF Roll off signals from detector in 0.001 μF Power amplifier feedback decoupling, sets low frequency supply rejection 0.1 μF AM detector bias resistor  Tuning Capacitor Specificati 0.0 μF Roll off signals from detector in 0.0 μF Power amplifier feedback decoupling 0.1 μF AM band to prevent radiation Power amplifier feedback decoupling 0.1 μF AM band to prevent radiation Power amplifier feedback decoupling 0.1 μF AM detector bias resistor  Tuning Capacitor Specificati 0.0 μF AM antenna 1 mV/meter induces approximately 100 μV open circuit at the secondary TOKO RWO-6A5105 or equivalent Toko America 1250 Feehanville Drive Mount Prospect, IL 60056 (312) 297-0070  TL/H/7909-9  1. N = 3½T, inner 5 mm  4 μH, N = 4½T, Qu = 70  1. N = 2½T, inner 5 mm  4 μH, N = 4½T, Qu = 70  1. N = 2½T, inner 5 mm  4 μH, N = 4½T, Qu = 70  1. N = 2½T, inner 5 mm  4 μH, N = 4½T, Qu = 70  1. N = 2½T, inner 5 mm  4 μH, N = 4½T, Qu = 70  1. N = 2½T, inner 5 mm  4 μH, N = 4½T, Qu = 70  200 Lake Park Drive Smyrna, GA 30080$	0.1 μF Antenna coupling capacitor C19 0.01 μF FM IF decoupling capacitors C7 0.005 μF AM smoothing/FM de-emphasis C8 network, de-emphasis pole is given by. R10  f1 $\cong$ 1 $2\pi$ (C6 + C9) $(\frac{R4}{R4} + R6)$ R1  10 μF Regulator decoupling capacitor 0.1 μF Regulator decoupling capacitor 0.1 μF Regulator decoupling capacitor 10 μF AC coupling to volume control R3 0.1 μF Power supply decoupling R3 0.1 μF Audio amplifier input coupling R6 0.001 μF If AM band to prevent radiation C18 0.001 μF Power amplifier feedback decoupling, sets low frequency supply rejection D1  16k AM detector bias resistor  Tuning Capacitor Specifications  40 pF max 5.0 pF min FM 20 pF max 4.5 pF min TOKO CY2-22124PT  5 pF ax 5.0 pF min TOKO CY2-22124PT  10 y > 80 @ F = 796 kHz AM antenna 1 mV/meter induces approximately 100 μV open circuit at the secondary  10 y > 80 @ F = 796 kHz TOKO RWO-6A5105 or equivalent Toko America 1250 Feehanville Drive Mount Prospect, IL 60056 (312) 297-0070  10 y = 2 y/π, inner = 5 mm  11	0.1 $\mu F$ 0.01 $\mu F$ 0.01 $\mu F$ FM IF decoupling capacitors C7 10 $\mu F$ 0.005 $\mu F$ AM smoothing/FM de-emphasis C8 0.1 $\mu F$ network, de-emphasis pole is given by.  F1 $\simeq \frac{1}{2\pi (C6 + C9) \left(\frac{R4}{R4 + R6}\right)}$ C21 C250 $\mu F$ Regulator decoupling capacitor C1. $\mu F$ Regulator decoupling capacitor R2 C21 C250 $\mu F$ R1 C82 C21 C250 $\mu F$ R2 C21 C250 $\mu F$ R3 S66 C21 C26 C21 C250 $\mu F$ R1 C82 C21 C250 $\mu F$ R2 C24 C250 $\mu F$ R3 S66 C28 C20 C21 C250 $\mu F$ R4 C82 C24 C250 $\mu F$ R3 S66 C28 C20 C21 C250 $\mu F$ R4 C82 C26 C21 C250 $\mu F$ R5 C82 C20 C21 C250 $\mu F$ R6 C82 C22 C21 C250 $\mu F$ R6 C21 C250 $\mu F$ R6 C82 C21 C250 $\mu F$ R1 C82 C21 C250 $\mu F$ R2 C24 C24 C24 C24 C24 C24 C25	

## **Layout Considerations**

#### AM SECTION

Most problems in an AM radio design are associated with radiation of undesired signals to the loopstick. Depending on the source, this radiation can cause a variety of problems including tweet, poor signal-to-noise, and low frequency oscillation (motor boating). Although the level of radiation from the LM1868 is low, the overall radio performance can be degraded by improper PCB layout. Listed below are layout considerations association with common problems.

- 1. **Tweet:** Locate the loopstick as far as possible from detector components C6, C9, R4, and R5. Orient C6, C9, R4, and R5 parallel to the axis of the loopstick. Return R8, C6, C9, and C19 to a separate ground run (see Typical Application PCB).
- 2. **Poor Signal-to-Noise/Low Frequency Oscillation:** Twist speaker leads. Orient R10 and C20 parallel to the axis of the loopstick. Locate C11 away from the loopstick.



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In general, radiation results from current flowing in a loop. In case 1 this current loop results from decoupling detector harmonics at pin 17; while in case 2, the current loop results from decoupling noise at the output of the audio amplifier and the output of the regulator. The level of radiation picked up by the loopstick is approximately proportional to: 1)  $1/r^3$ ; where r is the distance from the center of the loopstick to the center of the current loop; 2) SIN  $\theta$ , where  $\theta$  is the angle between the plane of the current loop and the axis of the loopstick; 3) I, the current flowing in the loop; and 4) A, the cross-sectional area of the current loop.

Pickup is kept low by short leads (low A), proper orientation ( $\theta \simeq 0$  so SIN  $\theta \simeq 0$ ), maximizing distance from sources to loopstick, and keeping current levels low.

### FM SECTION

The pinout of the LM1868 has been chosen to minimize layout problems, however some care in layout is required to insure stability. The input source ground should return to C4 ground. Capacitors C13 and C18 form the return path for signal currents flowing in the quadrature coil. They should connect directly to the proper pins with short PC traces (see Typical Application PCB). The quadrature coil and input circuitry should be separated from each other as far as possible.

## **AUDIO AMPLIFIER**

The standard layout considerations for audio amplifiers apply to the LM1868, that is: positive and negative inputs should be returned to the same ground point, and leads to the high frequency load should be kept short. In the case of the LM1868 this means returning the volume control ground (R6) to the same ground point as C17, and keeping the leads to C20 and R10 short.

## Circuit Description (See Equivalent Schematic)

#### AM SECTION

The AM section consists of a mixer stage, a separate local oscillator, an IF gain block, an envelope detector, AGC circuits for controlling the IF and mixer gains, and a switching circuit which disables the AM section in the FM mode.

Signals from the antenna are AC-coupled into pin 7, the mixer input. This stage consists of a common-emitter amplifier driving a differential amp which is switched by the local oscillator. With no mixer AGC, the current in the mixer is 330  $\mu\text{A}$ ; as the AGC is applied, the mixer current drops, decreasing the gain, and also the input impedance drops, reducing the signal at the input. The differential amp connected to pin 8 forms the local oscillator. Bias resistors are arranged to present a negative impedance at pin 8. The frequency of oscillation is determined by the tank circuit, the peak-to-peak amplitude is approximately 300  $\mu\text{A}$  times the impedance at pin 8 in parallel with 8k2.

After passing through the ceramic filter, the IF signals are applied to the IF input. Signals at pin 11 are amplified by two AGC controlled common-emitter stages and then applied to the PNP output stage connected to pin 13. Biasing is arranged so that the current in the first two stages is set by the difference between a 250  $\mu$ A current source and the Darlington device connected to pin 12.

When the AGC threshold is exceeded, the Darlington device turns ON, steering current away from the IF into ground, reducing the IF gain. Current in the IF is monitored by the mixer AGC circuit. When the current in the IF has dropped to 30  $\mu\text{A}$ , corresponding to 30 dB gain reduction in the IF, the mixer AGC line begins to draw current. This causes the mixer current and input impedance to drop, as previously described.

The IF output is level shifted and then peak detected at detector cap C1. By loading C1 with only the base current of the following device, detector currents are kept low. Drive from the AGC is taken at pin 14, while the AM detector output is summed with the FM detector output at pin 17.

## FM SECTION

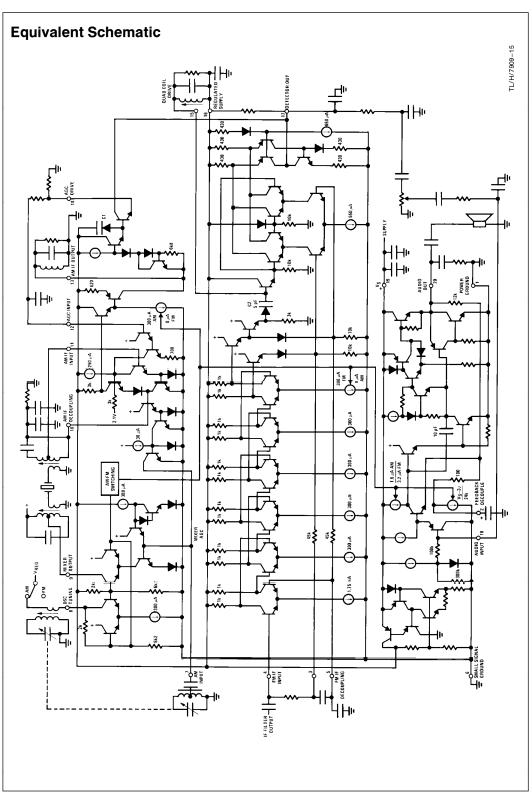
The FM section is composed of a 6-stage limiting IF driving a quadrature detector. The IF stages are identical with the exceptions of the input stage, which is run at higher current to reduce noise, and the last stage, which is switched OFF in the AM mode. The quadrature detector collectors drive a level shift arrangement which allows the detector output load to be connected to the regulated supply.

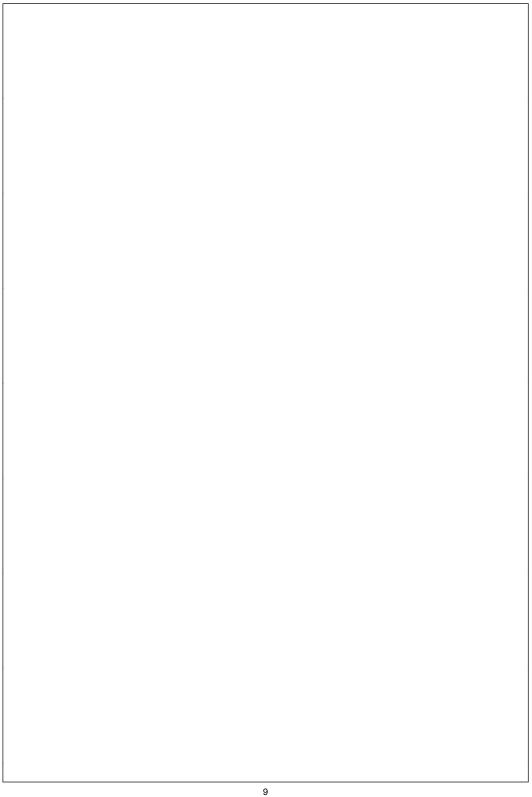
## **AUDIO AMPLIFIER**

The audio amplifier has an internally set voltage gain of 120. The bandwidth of the audio amplifier is reduced in the AM mode so as to reduce the output noise falling in the AM band. The bandwidth reduction is accomplished by reducing the current in the input stage.

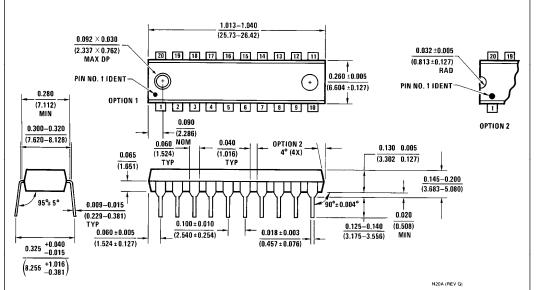
### REGULATOR

A series pass regulator provides biasing for the AM and FM sections. Use of a PNP pass device allows the supply to drop to within a few hundred millivolts of the regulator output and still be in regulation.





# Physical Dimensions inches (millimeters)



Molded Dual-In-Line Package (N) Order Number LM1868N NS Package Number N20A

## LIFE SUPPORT POLICY

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